Agreement

Concerning the Adoption of Harmonized Technical United Nations Regulations for Wheeled Vehicles, Equipment and Parts which can be Fitted and/or be Used on Wheeled Vehicles and the Conditions for Reciprocal Recognition of Approvals Granted on the Basis of these United Nations Regulations

(Revision 3, including the amendments which entered into force on 14 September 2017)

Addendum 48 – UN Regulation No. 49

Revision 5 - Amendment 6

Supplement 9 to the 05 series of amendments – Date of entry into force: 19 July 2018

Uniform provisions concerning the measures to be taken against the emission of gaseous and particulate pollutants from compression-ignition engines and positive ignition engines for use in vehicles

This document is meant purely as documentation tool. The authentic and legal binding text is: ECE/TRANS/WP.29/2017/129.

UNITED NATIONS

* Former titles of the Agreement:
Agreement concerning the Adoption of Uniform Conditions of Approval and Reciprocal Recognition of Approval for Motor Vehicle Equipment and Parts, done at Geneva on 20 March 1958 (original version);
Agreement concerning the Adoption of Uniform Technical Prescriptions for Wheeled Vehicles, Equipment and Parts which can be Fitted and/or be Used on Wheeled Vehicles and the Conditions for Reciprocal Recognition of Approvals Granted on the Basis of these Prescriptions, done at Geneva on 5 October 1995 (Revision 2).
Annex 4B

Paragraph 7.8.4., amend to read:

"7.8.4. Drift verification

As soon as practical but no later than 30 minutes after the test cycle is complete or during the soak period (for (b) only), the zero and span responses of the gaseous analyser ranges used shall be determined. For the purpose of this paragraph, test cycle is defined as follows:

(a) For the WHTC: the complete sequence cold – soak – hot;
(b) For the WHTC hot start test (paragraph 6.6.): the sequence soak – hot;
(c) For the multiple regeneration WHTC hot start test (paragraph 6.6.): the total number of hot start tests;
(d) For the WHSC: the test cycle.

The following provisions apply for analyzer drift:

(a) The pre-test zero and span and post-test zero and span responses may be directly inserted into equation 66 of paragraph 8.6.1. without determining the drift;
(b) If the drift between the pre-test and post-test results is less than 1 per cent of full scale, the measured concentrations may be used uncorrected or may be corrected for drift according to paragraph 8.6.1. of this annex;
(c) If the drift difference between the pre-test and post-test results is equal to or greater than 1 per cent of full scale, the test shall be voided or the measured concentrations shall be corrected for drift according to paragraph 8.6.1. of this annex."

Paragraph 8.4.1.7., amend to read:

"8.4.1.7. Carbon balance method

This involves exhaust mass calculation from the fuel flow and the gaseous exhaust components that include carbon. The calculation of the instantaneous exhaust gas mass flow is as follows:

\[
q_{\text{new,i}} = q_{\text{inf,i}} \times \left( \frac{w_{\text{BET}}^2 \times 1.4}{(1.0828 \times w_{\text{BET}} + k_{\text{id}} \times k_{c}) \times k_{c}} \right) \left( 1 + \frac{H_{a}}{1000} \right) + 1 \quad (33)
\]

With

\[
k_{c} = (c_{\text{CO2d}} - c_{\text{CO2d,a}}) \times 0.5441 + c_{\text{COd}}/18522 + c_{\text{HCw}}/17355 \quad (34)
\]

And

\[
k_{\text{id}} = -0.055586 \times w_{\text{ALF}} + 0.0080021 \times w_{\text{DEL}} + 0.0070046 \times w_{\text{EPS}} \quad (35)
\]

Where:

- \(q_{\text{inf,i}}\) is the instantaneous fuel mass flow rate, kg/s
- \(H_{a}\) is the intake air humidity, g water per kg dry air
- \(w_{\text{BET}}\) is the carbon content of the fuel, per cent mass
- \(w_{\text{ALF}}\) is the hydrogen content of the fuel, per cent mass
$w_{\text{DEL}}$ is the nitrogen content of the fuel, per cent mass

$w_{\text{EPS}}$ is the oxygen content of the fuel, per cent mass

$c_{\text{CO}_2}$ is the dry CO$_2$ concentration, per cent

$c_{\text{CO}_2a}$ is the dry CO$_2$ concentration of the intake air, per cent

$c_{\text{CO}}$ is the dry CO concentration, ppm

$c_{\text{HCw}}$ is the wet HC concentration, ppm

*Paragraph 9.3.9.4.1.*, amend to read:

"9.3.9.4.1. Sample dryer efficiency

For dry CLD analyzers, it shall be demonstrated that for the highest expected water vapour concentration $H_m$ (see paragraph 9.3.9.2.2.), the sample dryer maintains CLD humidity at $\leq 5$ g water/kg dry air (or about 0.8 volume per cent H$_2$O), which is 100 per cent relative humidity at 3.9 °C and 101.3 kPa. This humidity specification is also equivalent to about 25 per cent relative humidity at 25 °C and 101.3 kPa. This may be demonstrated by measuring the temperature at the outlet of a thermal dehumidifier, or by measuring humidity at a point just upstream of the CLD. Humidity of the CLD exhaust might also be measured as long as the only flow into the CLD is the flow from the dehumidifier."

*Paragraph 9.4.2.*, amend to read:

"9.4.2. General requirements of the dilution system

The determination of the particulates requires dilution of the sample with filtered ambient air, synthetic air or nitrogen (the diluent). The dilution system shall be set as follows:

(a) Completely eliminate water condensation in the dilution and sampling systems;

(b) Maintain the temperature of the diluted exhaust gas between 315 K (42 °C) and 325 K (52 °C) within 20 cm upstream or downstream of the filter holder(s);

(c) The diluent temperature shall be between 293 K and 325 K (20 °C to 52 °C) in close proximity to the entrance into the dilution tunnel;

(d) The minimum dilution ratio shall be within the range of 5:1 to 7:1 and at least 2:1 for the primary dilution stage based on the maximum engine exhaust flow rate;

(e) For a partial flow dilution system, the residence time in the system from the point of diluent introduction to the filter holder(s) shall be between 0.5 and 5 seconds;

(f) For a full flow dilution system, the overall residence time in the system from the point of diluent introduction to the filter holder(s) shall be between 1 and 5 seconds, and the residence time in the secondary dilution system, if used, from the point of secondary diluent introduction to the filter holder(s) shall be at least 0.5 seconds.

Dehumidifying the diluent before entering the dilution system is permitted, and especially useful if diluent humidity is high."
Paragraph 9.5.5., amend to read:

"9.5.5. Total system verification

The total accuracy of the CVS sampling system and analytical system shall be determined by introducing a known mass of a pollutant gas into the system while it is being operated in the normal manner. The pollutant is analyzed, and the mass calculated according to paragraph 8.5.2.3. except in the case of propane where a \( u \) factor of 0.000507 is used in place of 0.000483 for HC. Either of the following two techniques shall be used."

Appendix 4, paragraph A.4.2., amend to read:

"A.4.2. Regression analysis

The slope of the regression shall be calculated as follows:

\[
a_i = \frac{\sum_{i=1}^{n} (y_i - \bar{y}) \times (x_i - \bar{x})}{\sum_{i=1}^{n} (x_i - \bar{x})^2}
\]

(94)

The \( y \) intercept of the regression shall be calculated as follows:

\[
a_0 = \bar{y} - (a_1 \times \bar{x})
\]

(95)

The standard error of estimate (SEE) shall be calculated as follows:

\[
SEE = \sqrt{\frac{\sum_{i=1}^{n} [y_i - a_0 - (a_1 \times x_i)]^2}{n-2}}
\]

(96)

The coefficient of determination shall be calculated as follows:

\[
r^2 = 1 - \frac{\sum_{i=1}^{n} [y_i - a_0 - (a_1 \times x_i)]^2}{\sum_{i=1}^{n} (y_i - \bar{y})^2}
\]

(97)