Progress Report

DTP Subgroup

Lab Process Internal Combustion Engines

(LabProcICE)

Geneva, 6.6.2012

DTP Subgroup LabProcICE

WLTP 10th DTP Meeting Geneva, 6.6.2012

- 1) State of the working progress
- 2) Roadmap & validation phases 2 and 3
- 3) Issues on DTP level
- 4) Work in progress items / proposals / open issues
- 5) Next steps

Meetings since DTP9

• 15.05.2012 Telephone Conference

• <u>22.05.2012</u> Brussels workshop

minutes: LabProcICE-133

OIL, gtr draft, definitions

Open issues list

<u>LabProcICE-111</u> (will be updated soon)

Note: additional LabProcICE <u>open issues are listed in the gtr draft</u> documents, see comments of S. Dubuc (Drafting Coordinator).

gtr draft

Several draft tel/web conferences with LabProcICE experts organized by Serge Dubuc (DC)

Gtr draft version 1 (see DC documents WLTP-2012-015 /-.../-023)

Annexes:

l: drive cycles (incl. mode construction)

II: gear selection & shift points

III: reference fuels

IV: road load determination

V: test equipment, calibrations

VI: test procedure, test conditions

VII: calculations

VIII: electrified vehicles

IX: system equivalency



Current status:

- DC documents (WLTP-2012-002 /-003 /-004)
- Gaseous Fuel definitions (GFV-18-02)

WP.29:

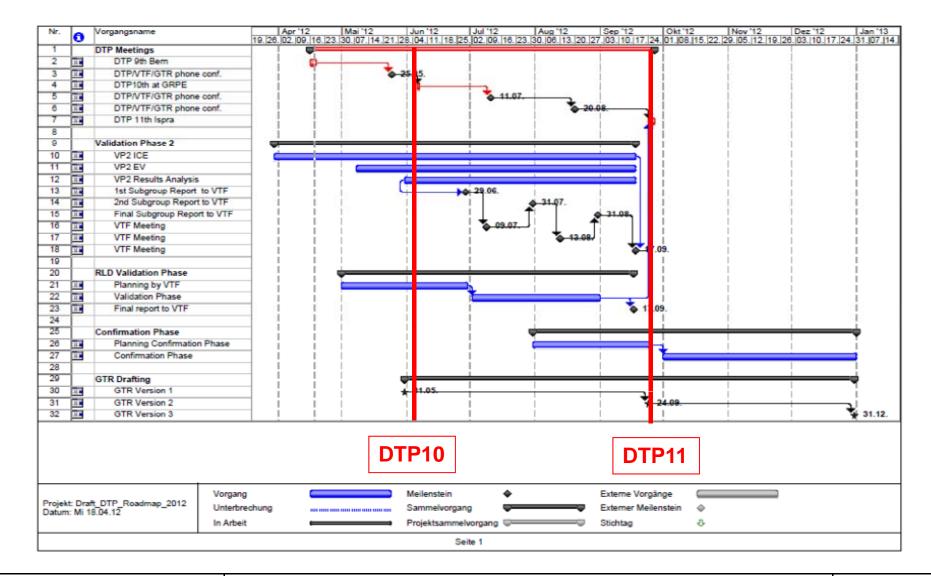
Task Force Group under GRPE to develop a frame system of terms, definitions and classifications regarding vehicle propulsion systems (see <u>WP.29-156-26</u>)

Next steps:

- Separate meetings with DC and representatives from all subgroups will be scheduled by DC
- Definitions will be imported into a database



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Open roadmap issues affecting LabProcICE

Concerns regarding the ability to achieve evaluation of validation 2 results within the given timeframe (DTP11, Sept 2012)

- → interaction & responsibilities LabProcICE / VTF?
- → data availability, status of provided data?
- → all decisions taken at DTP11? start of confirmation tests in Oct 2012?

Update from DTP/VTF meeting 05.06.2012:

Proposal of WLTP steering group welcomed

- → possible extension of validation 2 evaluation until Jan 2013 (DTP12)
- → start of confirmation / round robin in 2013

Validation phase 2

VTF documents provided by LabProcICE and continuously reviewed:

- Assessment criteria
- Parameter setting list
- Excel data sheet for reporting of results
- Global Test Matrix
 - → reminder: final check if the selected vehicles and the intended tests will deliver sufficient results to come to decisions regarding all evaluation issues
- Evaluation Issues for Validation 2
 - → Guidance document <u>DTP-09-10</u>

Validation phase 3 - road load determination

- Roadmap: July September 2012
- Coordination: VTF key responsibility Japan
- Parameter setting list:

first draft provided by Japan

→ to be reviewed by LabProcICE RLD experts



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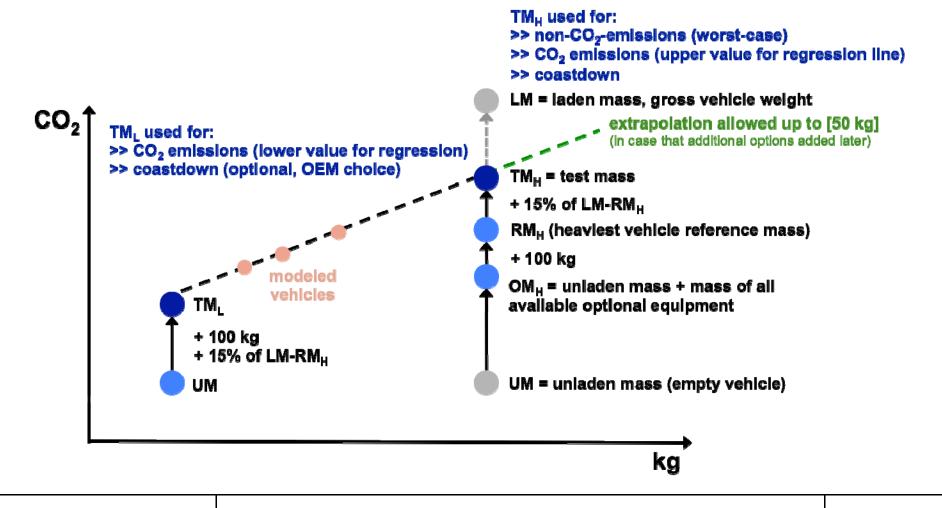
Test mass / inertia classes / vehicle selection

(see <u>DTP-10-02</u>)

Combined approach includes:

- (1) vehicle test mass improved definition (incl. optional equipment, luggage/payload)
- (2) step-less inertia
- (3) optional body parts influencing the aerodynamics
- → Testing worst case and in addition best case (if requested by manufacturer)

DTP-10-02, figure 1:



Tyre selection criteria

- → excluded from general approach
- → follow RLD selection criteria in both cases (TM_h, TM_l) (note: scrutiny reservation by Japan)

LabProcICE proposal:

- → Tyre from the worst rolling resistance class (defined by European tyre labeling directive, RR acc. to R117)
- → No distinction of tyres with different RR coefficients within the worst class
 → final decision based on ICCT study on the CO₂ impact of the RR
- → Approval extensions or the necessity of re-tests is no gtr issue



Comments/ proposals from Japan (DTP-10-xx) on tyre & vehicle selection

Aerodynamic options

- → Update of gtr draft (Annex IV on RLD)
- → <u>Discussions in draft expert and LabProcICE meetings:</u>

Items to be included in best / worst case approach (e. g. wheel rims, position of covers of air ventilation, retractable spoilers etc.)

→ proposals by **Japan** (DTP-10-xx) and **T&E**

Payload factors

Current proposal based on AEA report: M1 15%, N1 35%

Japan (LabProcICE-132):

→ N1 factor may differ significantly from 35% in Japan

India (<u>LabProcICE-128</u>):

→ Alignment of the M1 and N1 payload factors (esp. for LPW)

LabProcICE concluded:

- → Current payload factors proposal is still valid
- → All parties are requested to submit data to justify their counterproposals.
- → Discussion on DTP level based on validation 2 results and additional data



See initial discussion document by Bill Coleman (DTP-09-02rev1)

- → Analysis of family concepts in ECE R83.06
 - test families
 - definitions
 - modifications of the vehicle type
 - extensions to type approval
- → revision and redefinition of family parameters is necessary and possible

DTP9:

- → family concepts (or at least guidelines) should be part of the gtr
- → All contracting parties are asked for comments until DTP10



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Road Load Determination

Table of Running resistances (see <u>LabProcICE-121</u> by PSA)

- No updated proposal due to missing feedback from EU COM / JRC
- Reservation by EU COM:
 Default factors should represent worst case, use of table data should not be an incentive
- Indian comments (LabProcICE-128) will be considered in gtr draft

Other proposals (see <u>LabProcICE-120rev1</u> by Japan):

- Vehicle warming up for RLD / dyno load setting <u>.</u>
- •
- → discussion at RLD draft expert meetings / LabProcICE

Measurement equipment

Proportional fan

<u>Current proposal</u>: max. fan speed = max. speed of cycle (132 km/h)

(Note: separate requirements were set for validation 2: at least 100 km/h)

LabProcICE discussion:

- Concerns by Japan
- Automotive industry proposed to limit the max. fan speed to <u>120 km/h</u> for cost/benefit reasons: speeds 120-132 km/h only occur for seconds in cycle ←→ energy consumption and costs for new equipment.
 - → objection by NL

Proposal from automotive industry experts:

"Cooling fan specifications:

A current of air of variable speed shall be blown over the vehicle. The cooling fan shall have a maximum speed of at least 132 km/h. The linear velocity of the air at the outlet shall be ± 5 km/h or within ± 15 % of the corresponding roller speed, whichever is greater. At roller speeds of less than 10 km/h, air velocity may be zero."

Justification:

At maximum roller speed (132 km/h) air velocity has to be within 113 km/h and 152 km/h). This is a compromise between exact reproduction of ambient conditions and the technical realization of air flow in different test cells.



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Meeting schedule

- Small draft experts teams will continue work with DC
- Additional Tel/web conferences, e. g. for evaluation of validation phase 2 results
- Next face-to-face workshop: **04.- 06. September 2012** (tbc), Brussels (ACEA)

Thanks for your attention.

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