

# RESEARCH PROGRAM ON AN EMISSIONS TEST PROCEDURE FOR HEAVY DUTY HYBRIDS (HDH)

Development of Emissions and CO<sub>2</sub> Test Procedure for  
Heavy Duty Hybrid Vehicles

WP3: Non-electric HDHs

**Jonas Fredriksson**

Department of Signals and Systems  
Chalmers University of Technology  
Gothenburg, Sweden

# Content

- Introduction
- Work package 3-1
  - Method/Analysis
  - Results
- Work package 3-2
  - Method/Analysis
  - Results
- Summary

# Development of Emissions and CO2 Test Procedure for Heavy Duty Hybrid Vehicles

## **3. Extension of HILS to non-electrical hybrids, which are currently not covered by Kokujikan No.281.**

To May 2012 the following WP is to be carried out.

- Overview of possible other types of hybrids of interests and issues for HILS testing will be investigated. Information gathering. Proposal of which non-electric hybrids to include in the HILS method.
- Evaluate, using software models and simulation the possibilities of using HILS for assessment of quality factors of these hybrids.

# Tasks and timeplan

	<b><i>Work task description</i></b>	<b><i>Period (Start-end)</i></b>
WP 3	Extension to non-electrical hybrids	
WT 3.1	Technology overview and selection of scope	06/2011-10/2011
WT 3.2	Development of HIL elements (models) for non-electrical hybrids	10/2011-01/2012
WT 3.3	Test methods for input data to non-electrical component models	01/2012-02/2012
WT 3.4	Definition of control signals	01/2012-02/2012
WT 3.5	Alignment with HILS for HEV and verification	03/2012-04/2012

# Development of Emissions and CO2 Test Procedure for Heavy Duty Hybrid Vehicles

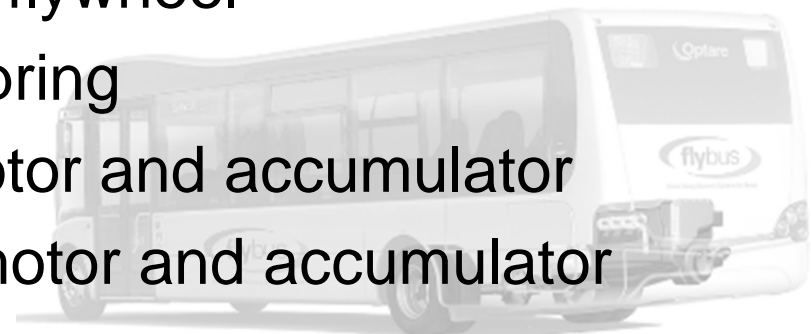
## **WT 3-1: Technology overview and selection of scope**

- Detailed analysis on what non-electric hybrid systems/components to be included in the HILS method. **Review of non-electric hybrid topologies** proposed in the literature, by OEMs and others. **Review of non-electric components**, such as flywheels, accumulators etc, used in non-electric powertrains proposed in the literature, by OEM and others. Together with OEMs and other partners decide which topologies that should be covered. Meetings with OEMs, will be co-planned with TU Graz and TU Wien in relation to WP 1-4 (TU Graz and TU Wien offer).
- The preliminary **result** is a **list of non-electric powertrain topologies** and a **list of components** that needs to be modeled.

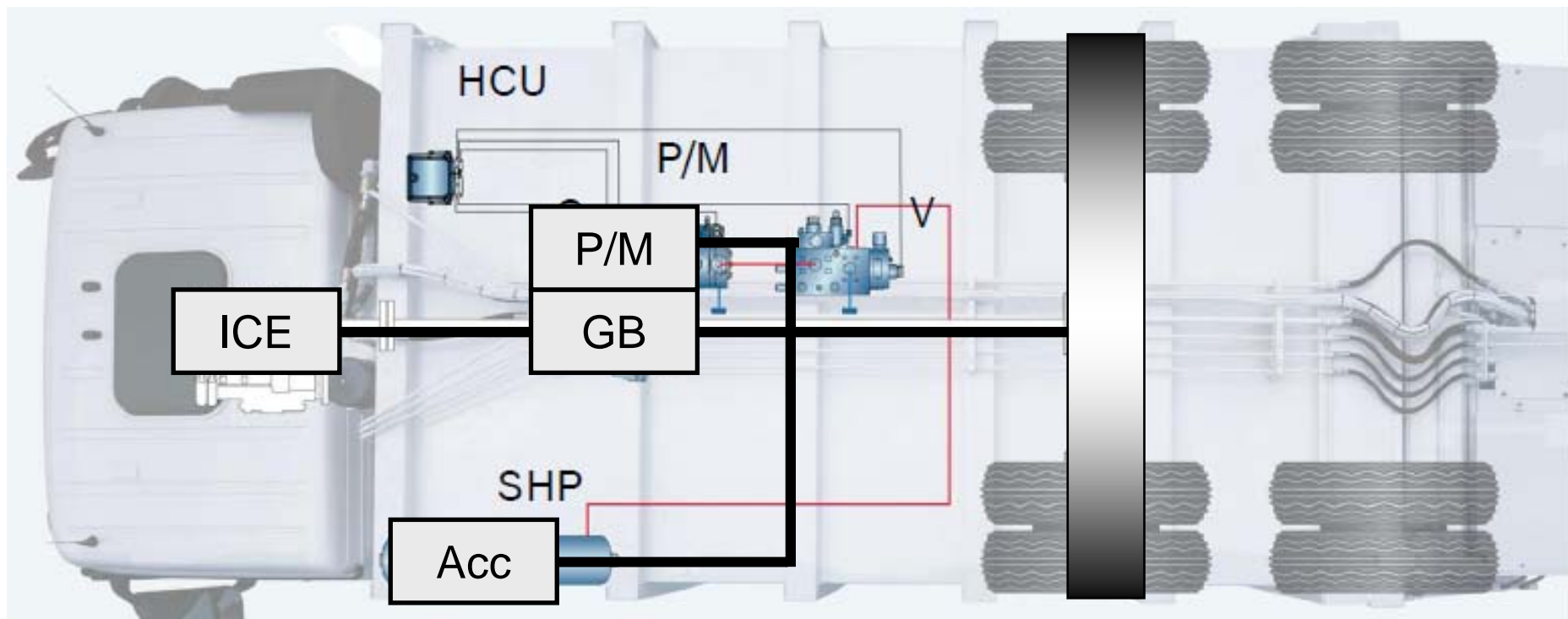
# Hybrid Powertrain Principles

## **Energy storage and converter**

- Electrochemical, generator/motor and battery
- Electrostatic, generator/motor and supercapacitor
- Electromagnetic, generator/motor and superconductor coil
- Kinetic, CVT and flywheel
- Kinetic, motor/generator and flywheel
- Potential, CVT and torsion spring
- Potential, hydraulic pump/motor and accumulator
- Potential, pneumatic pump/motor and accumulator



# Hydraulic pump/motor and accumulator

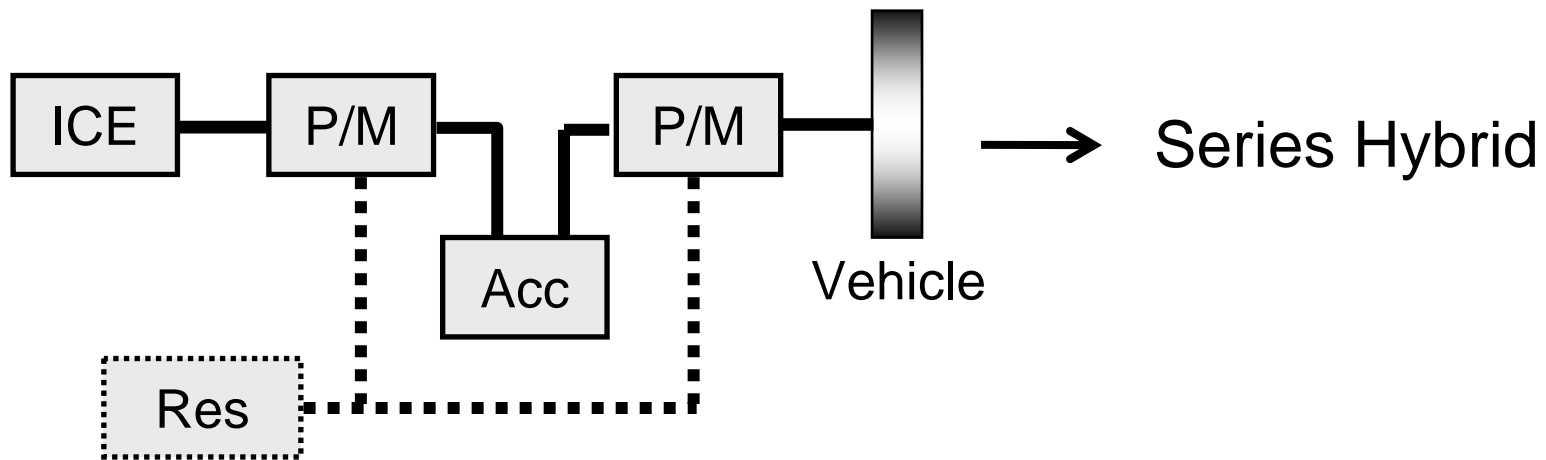
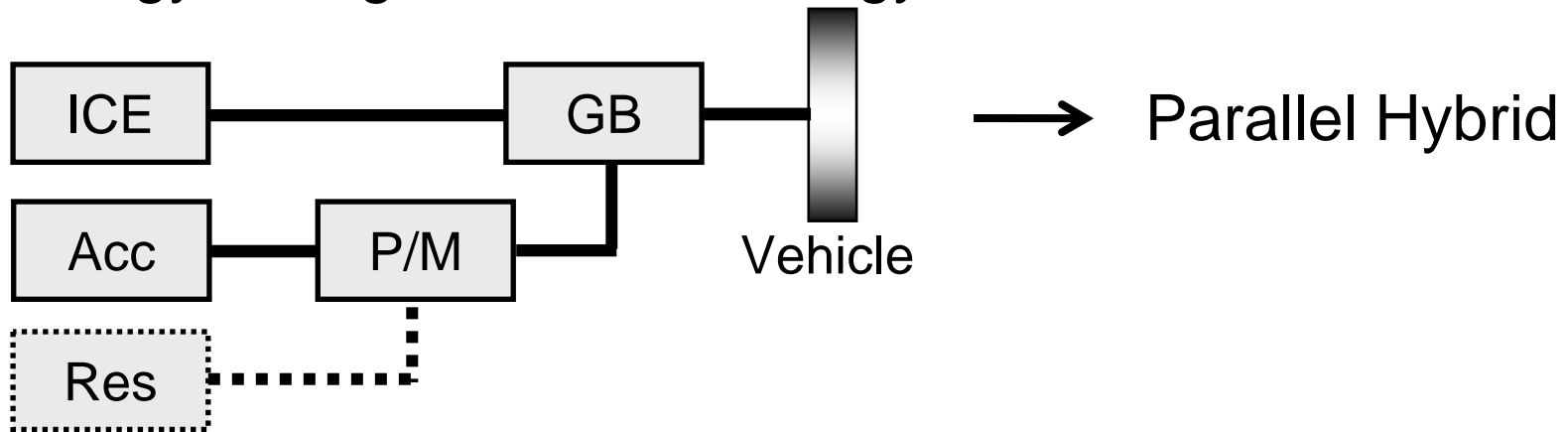


Vehicle

Rexroth HRB

# Hydraulic pump/motor and accumulator

- Energy storage: Potential energy



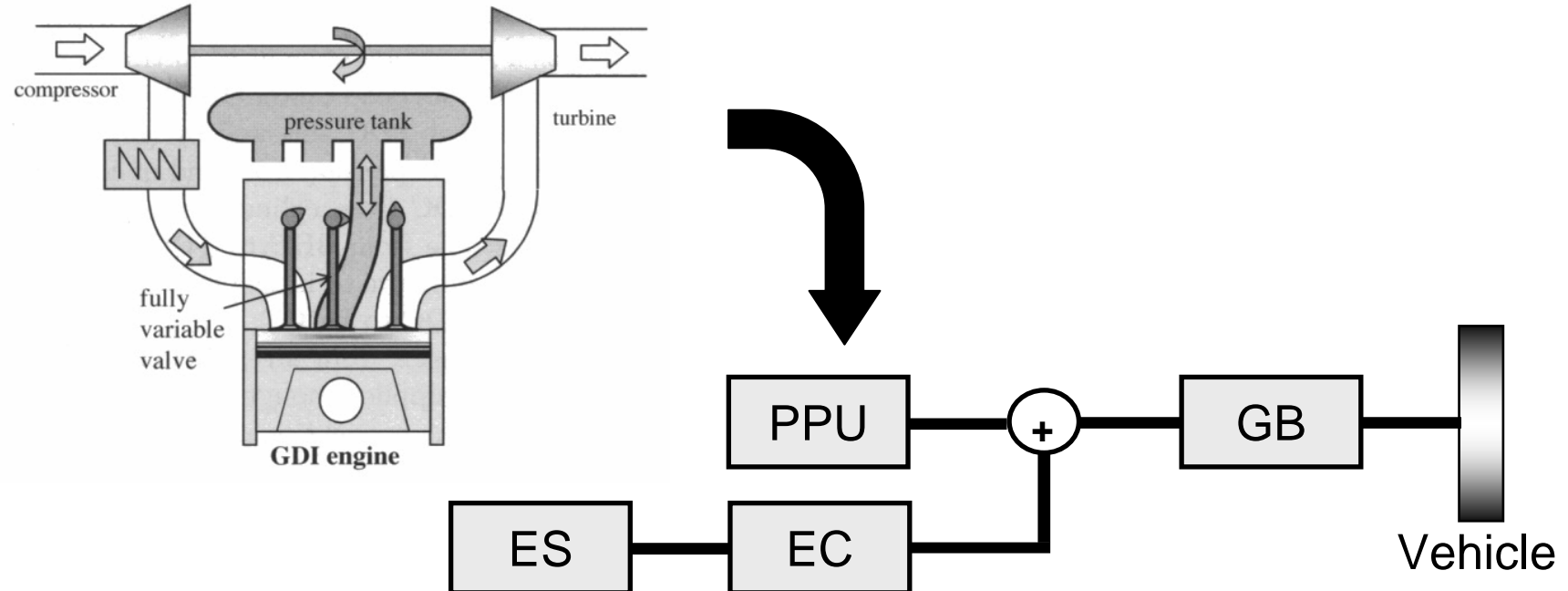


# Hydraulic pump/motor and accumulator

- Ford F150 and F350 Hydraulic Hybrid (Parallel)
- Eaton, Hydraulic Launch Assist (Parallel and Series)
- NRG Dynamix (Parallel and Series)
- Innas, Netherlands, (Series)
- Parker, Runwise system, (Parallel and Series)
- Bosch Rexroth, HRB (Parallel and series)
- Poclain Hydraulics, ADDIDRIVE Assist (Series, add-on to non-driven wheels)

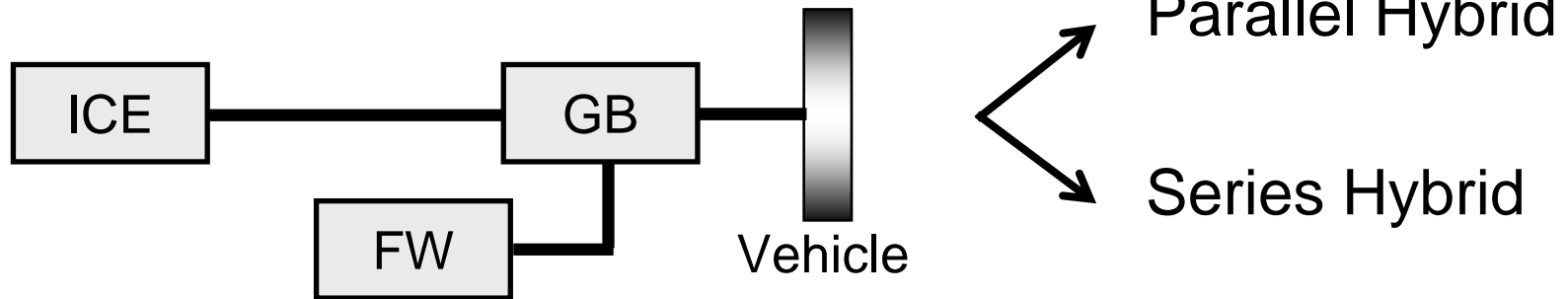
# Pneumatic pump/motor and accumulator

- Energy storage: Potential energy
  - Principle could be similar as for hydraulic hybrids
- Alternative: Hybrid engine concept:

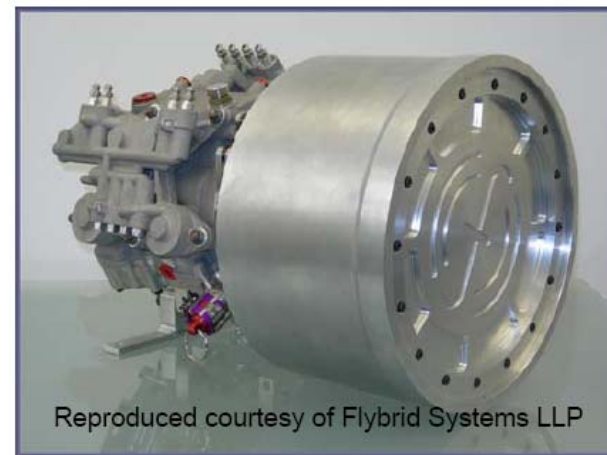


# CVT and flywheel

- Energy Storage: Kinetic energy

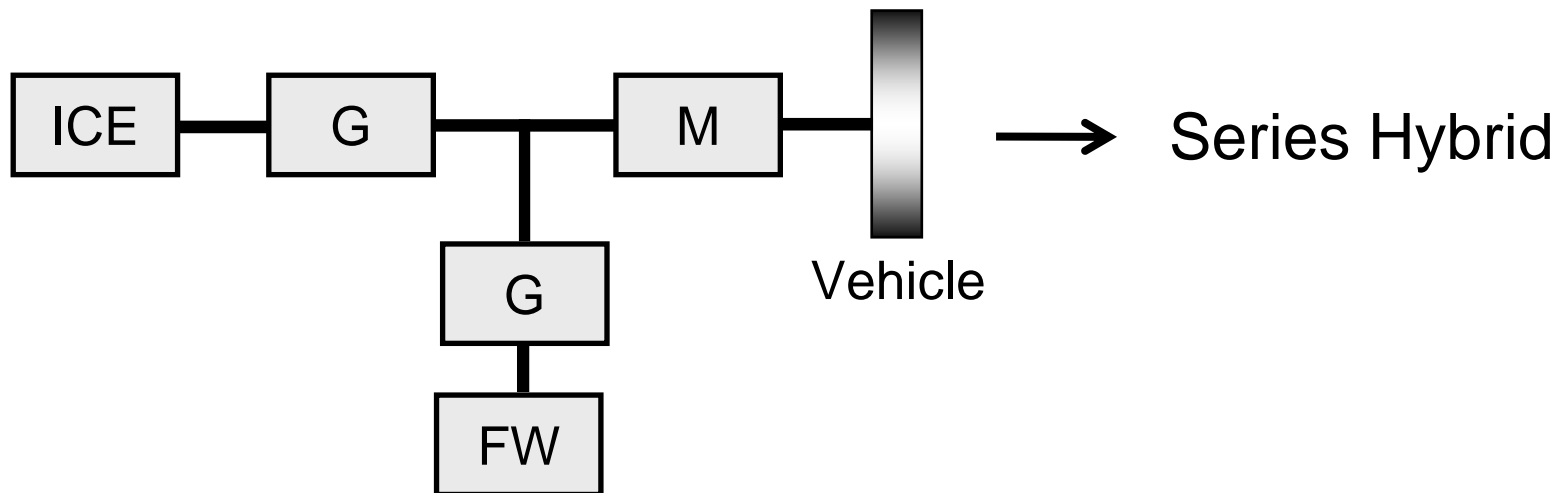


- Examples:
  - Formula 1
  - Flybrid
  - Torotrack for city bus



# Motor/generator and flywheel

- Energy storage: Kinetic energy



- Examples:
  - PhD thesis from Uppsala University, Sweden



# Results

- Non-electric hybrid powertrain topologies (concepts) fits well into the same categories as for electric hybrid powertrains
- Non-electric hybrid powertrains can be divided into:
  - Series powertrain topologies
  - Parallel powertrain topologies
  - Split powertrain topologies

# Interesting non-electric powertrain concepts:

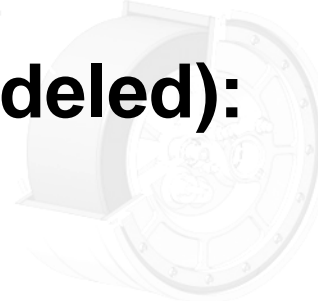
- CVT and flywheel
- Motor/generator and flywheel
- Hydraulic or (pneumatic) pump/motor and accumulator

# Results

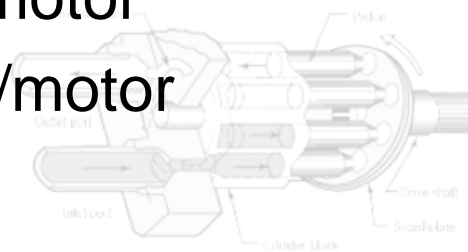
## Component list (to be modeled):

- Energy storages:
  - Flywheel
  - Hydraulic accumulators
  - Pneumatic accumulators
- Energy converters
  - CVT (transmission)
  - Hydraulic pump/motor
  - Pneumatic pump/motor

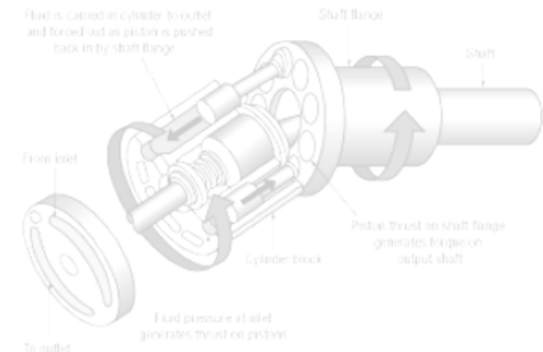
Flywheel in vacuum



Flywheel containment



(a) Swash-plate type, inline axial-piston type



(b) Bent-axis type, axial-piston type

# Development of Emissions and CO2 Test Procedure for Heavy Duty Hybrid Vehicles

## **WT 3-2: Development of HIL elements for non-electrical hybrid systems/components**

- Based on the list of topologies and components in WP 3-1, develop simple, representative **mathematical models** of the different powertrain components, such as actuators and energy buffers. The models will be implemented in a simulation software. All models will be documented.
- The result is a set of **simulation models of non-electric powertrain components**, which are suitable to use in a HILS setup.



# Components

- Energy storages:
  - Flywheel
  - Hydraulic accumulators
  - Pneumatic accumulators
- Energy converters
  - CVT (transmission)
  - Hydraulic pump/motor
  - Pneumatic pump/motor

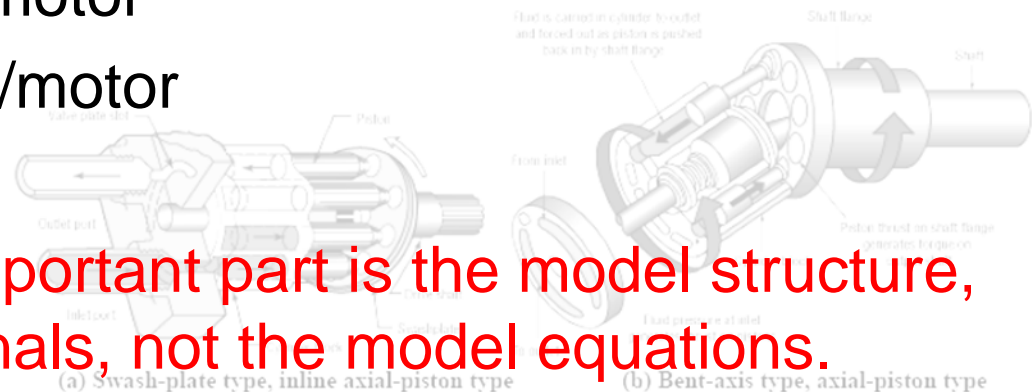
Flywheel in vacuum



Flywheel containment



- Notice: The most important part is the model structure, the input-output signals, not the model equations.



# Energy storages

- Flywheel
- Accumulators

Flywheel in vacuum  
Flywheel  
containing



Flywheel containment



- Notice: The similarity to the electric energy storage

# Flywheel

**Electric battery:**



**Flywheel:**



State-of-Charge

$$C \frac{dSOC}{dt} = -i$$

$$J \frac{d\omega}{dt} = -T - T_{loss}(\omega)$$

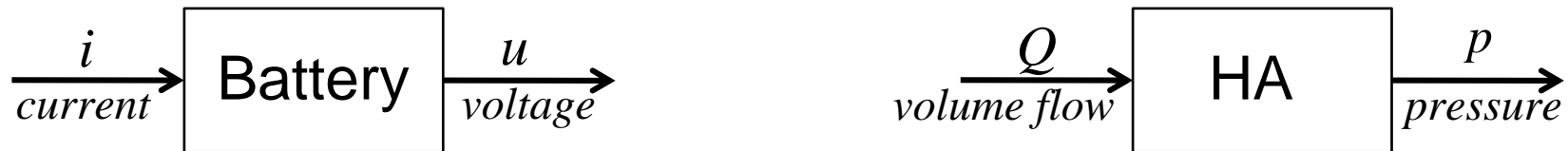
losses

$$u = u_{OCV}(SOC) - Ri$$

$T_{loss}(\omega)$  - Lookup table

# Accumulator

**Electric battery:**



State-of-Charge

$$C \frac{dSOC}{dt} = -i$$

$$\frac{dV_g}{dt} = Q \quad (\text{mass balance})$$

losses

$$u = u_{OCV}(SOC) - Ri$$

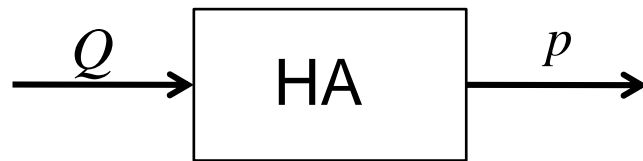
Temperature

$$p_g = \frac{m_g R_g \mathcal{G}_g(t)}{V_g(t)} \quad (\text{ideal gas law})$$

$$m_g c_v \frac{d\mathcal{G}_g}{dt} = -\frac{m_g R_g \mathcal{G}_g(t)}{V_g(t)} Q - hA_w (\mathcal{G}_g - \mathcal{G}_w)$$

(energy balance)

# Accumulators



Mass balance:  $\frac{dV_g}{dt} = Q$

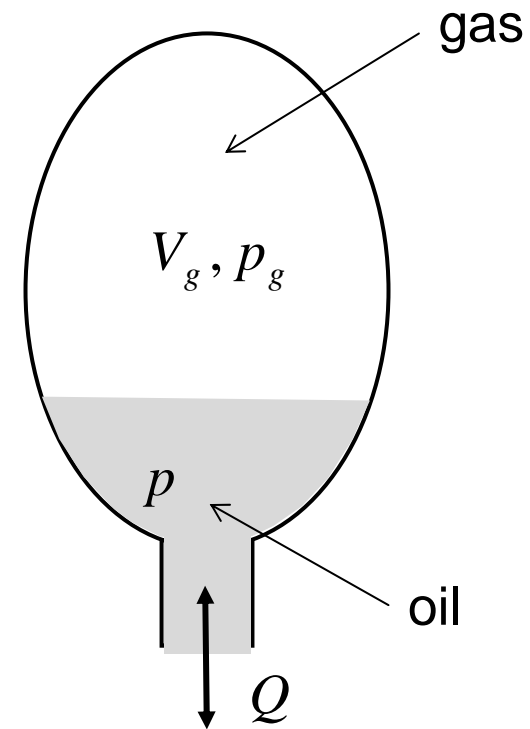
State-of-Charge

Ideal gas law:  $p_g = \frac{m_g R_g \mathcal{G}_g(t)}{V_g(t)}$

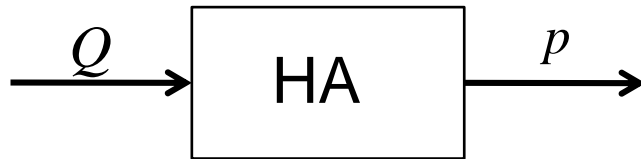
Temperature

Assumption ([1]):  $p \approx p_g$

Energy balance:  $m_g c_v \frac{d\mathcal{G}_g}{dt} = -\frac{m_g R_g \mathcal{G}_g(t)}{V_g(t)} Q - hA_w (\mathcal{G}_g - \mathcal{G}_w)$



# Accumulators



Mass balance:  $\frac{dV_g}{dt} = Q$

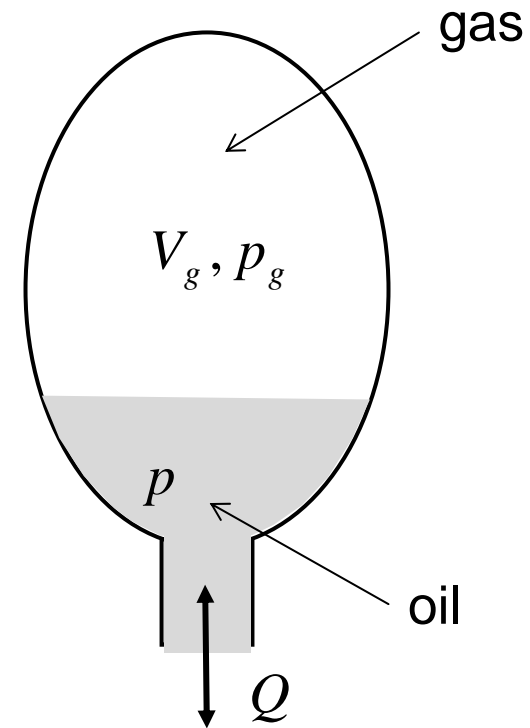
State-of-Charge

Ideal gas law:  $p_g = \frac{m_g R_g \mathcal{G}_g(t)}{V_g(t)}$

Temperature

Assumption ([1]):  $p \approx p_g$

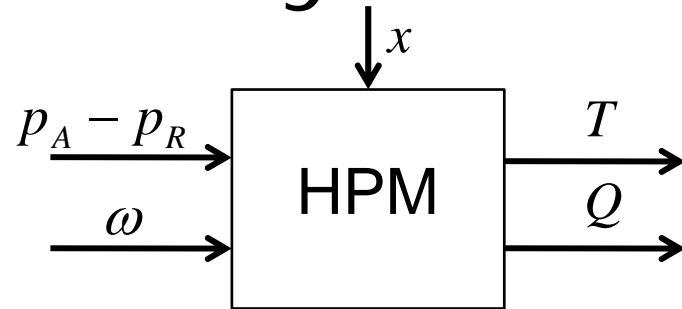
Energy balance:  $m_g c_v \frac{d\mathcal{G}_g}{dt} = -\frac{m_g R_g \mathcal{G}_g(t)}{V_g(t)} Q - hA_w (\mathcal{G}_g - \mathcal{G}_w)$



# Energy converters

- Hydraulic pump/motor
- CVT
  
- Notice: The similarity to the electric energy converter

# Hydraulic Pump/Motor



Pump:

$$Q = \eta_v x D \omega$$

Motor:

$$Q = x D \omega / \eta_v$$

Volumetric flow rate:

Torque:

$$T = \eta_t x D (p_A - p_R)$$

$$T = x D (p_A - p_R) / \eta_t$$

Efficiencies:

$$\eta_v = 1 - \frac{C_s}{xS} - \frac{p_A - p_R}{\beta} - \frac{C_{st}}{x\sigma}$$

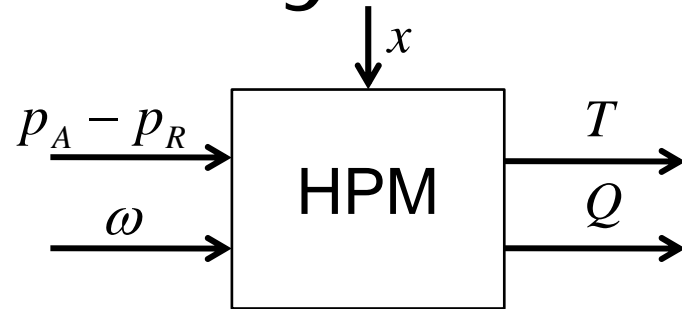
laminar loss  $\nearrow$   $\frac{C_s}{xS}$   $\nearrow$   $\frac{p_A - p_R}{\beta}$   $\nearrow$   $\frac{C_{st}}{x\sigma}$   
compressibility loss  $\nearrow$   $\frac{C_{st}}{x\sigma}$   $\nearrow$  turbulent loss

$$\eta_t = 1 - \frac{C_s S}{x} - \frac{C_f}{x} - C_h x^2 \sigma^2$$

viscous loss  $\nearrow$   $\frac{C_s S}{x}$   $\nearrow$   $\frac{C_f}{x}$   $\nearrow$   $C_h x^2 \sigma^2$   
friction loss  $\nearrow$   $C_h x^2 \sigma^2$   $\nearrow$  hydrodynamic loss



# Hydraulic Pump/Motor



Pump:

$$Q = \eta_v x D \omega$$

Motor:

$$Q = x D \omega / \eta_v$$

Volumetric flow rate:

Torque:

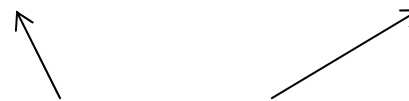
$$T = \eta_t x D (p_A - p_R)$$

$$T = x D (p_A - p_R) / \eta_t$$

Efficiencies:

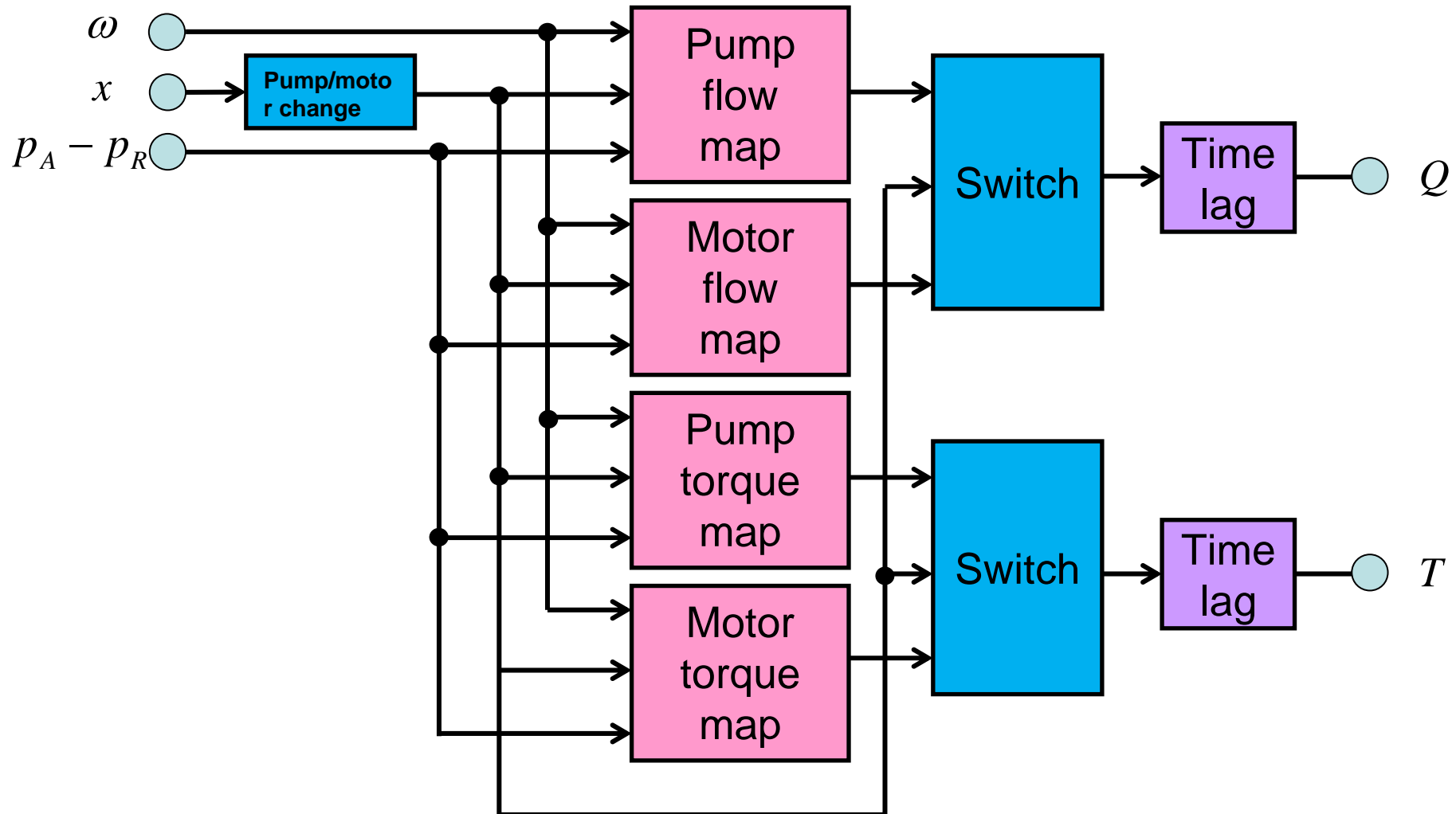
$$\eta_v = f(x, p_A - p_R, \omega)$$

$$\eta_t = f(x, p_A - p_R, \omega)$$



Lookup table

# Pump/motor Vs ...



# ... Vs Electric Motor Model

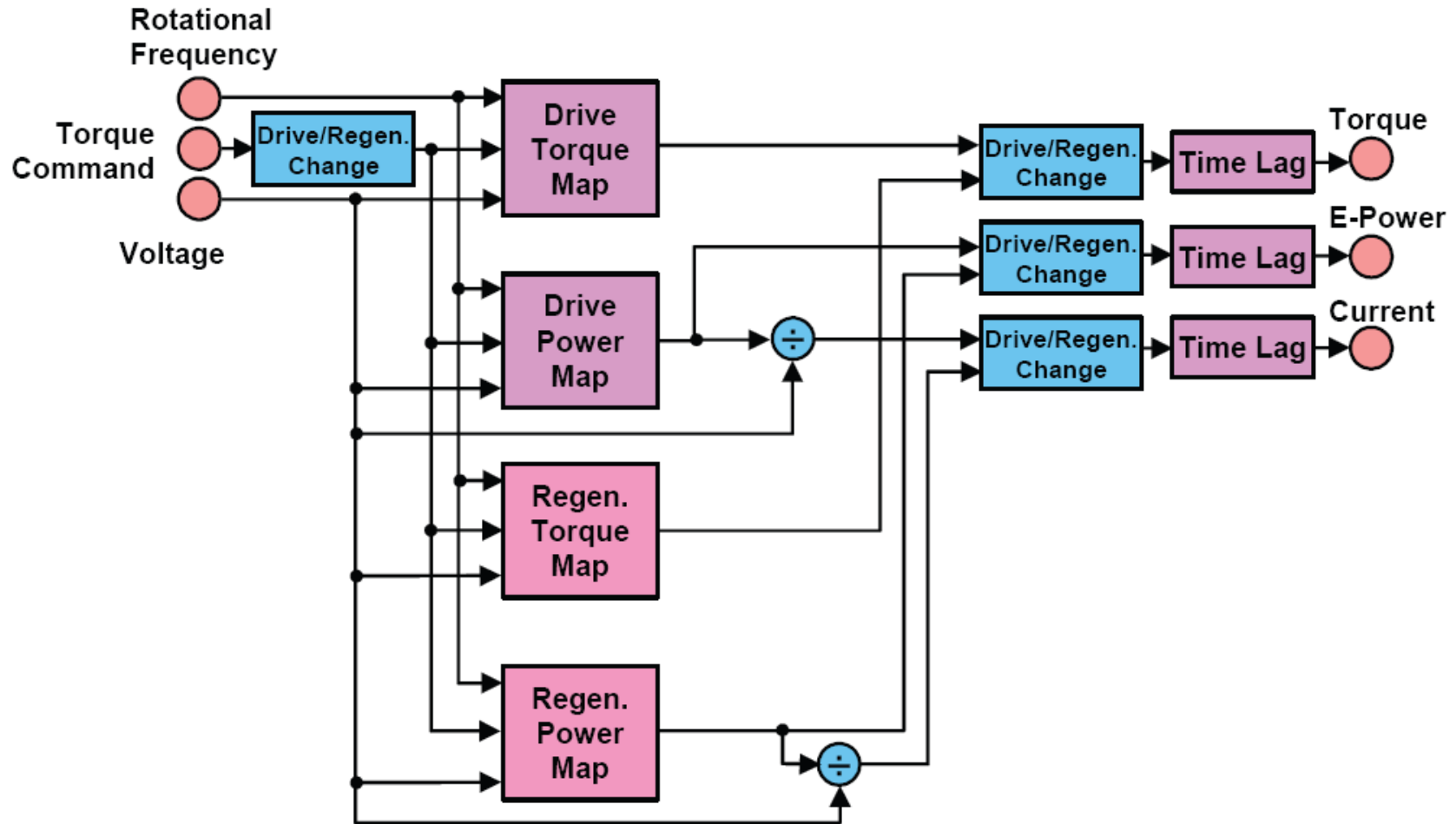
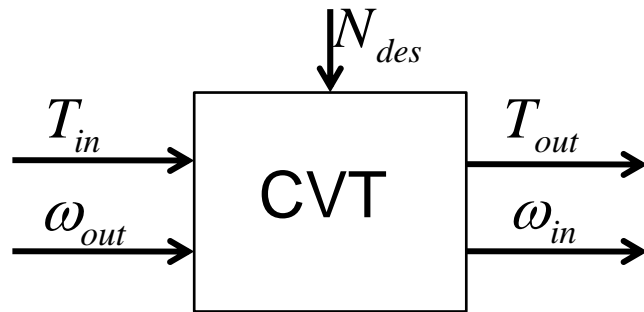


Fig. 3 Conceptual Diagram of Electric Motor Model

# CVT



Torque:  $T_{out} = NT_{in}\eta$

Efficiency:  $\eta = f(\omega_{out}, T_{out}, N)$

Lookup table



Speed:  $\omega_{in} = N\omega_{out}$

Gear ratio:  $\frac{dN}{dt} = -\frac{1}{T}(N - N_{des})$

# Results

- Mathematical models for
  - Flywheel
  - Accumulator
  - Pump/Motor
  - CVT

# Summary

- WT 3-1:
  - Non-electric hybrid powertrain topologies (concepts) fits well into the same categories as for electric hybrid powertrains
  -  HILS should be possible for non-electric HDHs
- WT 3-2:
  - Mathematical models for:
    - Flywheel
    - Accumulator 
    - Pump/Motor
    - CVT
  - Similar model structures as proposed in Kokujikan No. 281
- Work done according to time plan

# Next...

- Implementation
  - MATLAB/Simulink (Started)
- Verification (WT 3.3)
  - Data (Need to get real model data from suppliers or OEMs to verify model structure)
- System modelling
  - Incorporate into the Japanese open-source model
  - Controller design (Started, a simple rule based controller)

Thanks for your attention!

## Contact information

Jonas Fredriksson  
Department of Signals and Systems  
Chalmers University of Technology

[jonas.fredriksson@chalmers.se](mailto:jonas.fredriksson@chalmers.se)  
+46-31-772 1359