

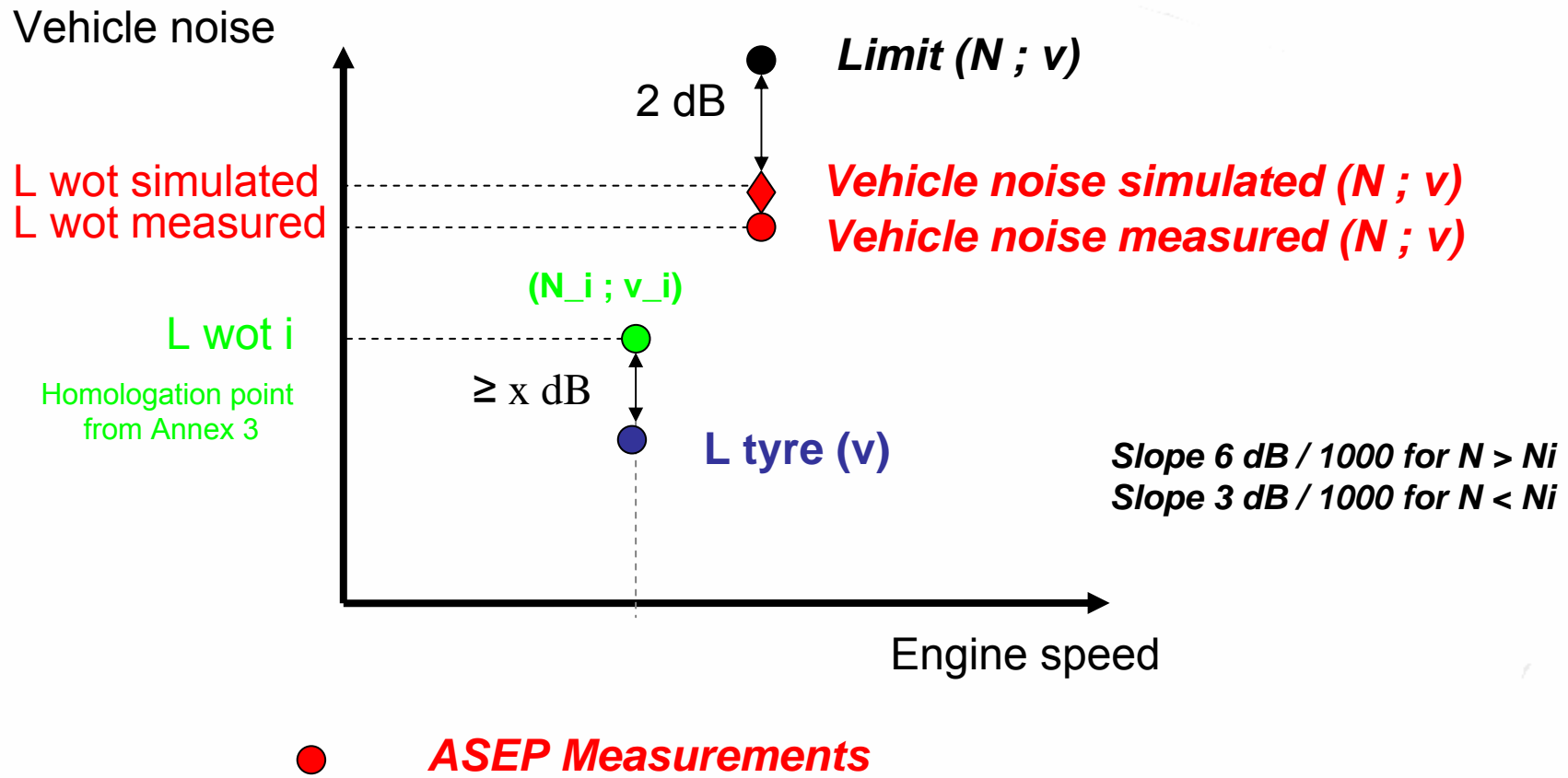
Additional Sound Emission Provisions

Can we simplify
France/German method ?

- Description of F/D proposal and J Proposal
- Limit line(s) instead of Limit Points –
A possibility to converge to Japan Proposal
- Tyre noise close to vehicle noise –
A possibility to solve the problem

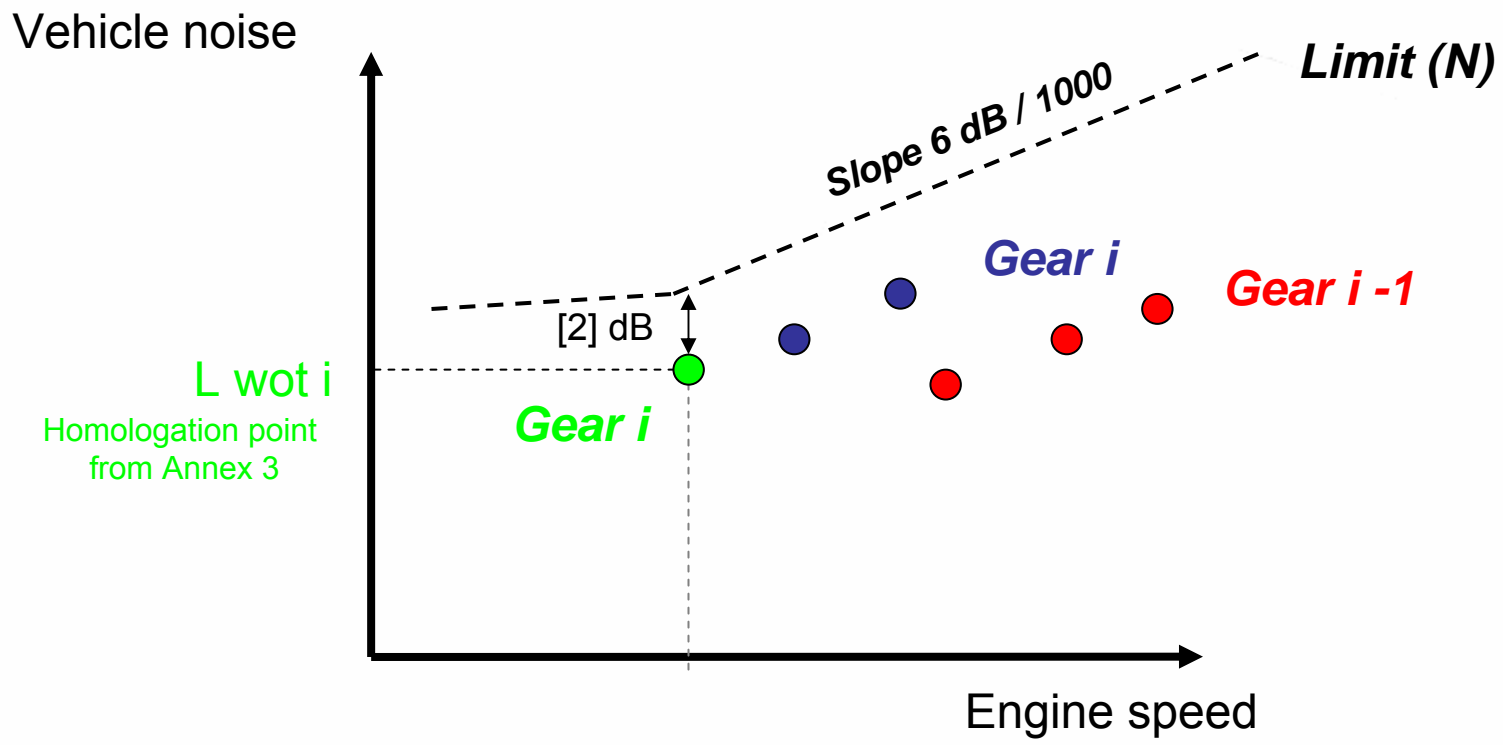
Presentation of actual F/D Proposal

Model :
 $L_{\text{tyre}} = L_{\text{tyre}}(v_{\text{ref}}) + a \cdot \log(v/v_{\text{ref}})$
 $L_{\text{engine expecting}} = L_{\text{engine}}(N_{\text{ref}}) + b(N - N_{\text{ref}})$
 $L_{\text{vehicle}}(N, v) = L_{\text{engine expecting}}(N) \ll + \gg L_{\text{tyre}}(v)$
 $L_{\text{limit}} = L_{\text{vehicle}}(N, v) + 2 \text{ dB}$



Presentation of actual Japan Proposal

Model :
 $L_{\text{vehicle expecting}} = L_{\text{wot } i} (N_{\text{ref}}) + b (N - N_{\text{ref}})$
 $L_{\text{limit}} = L_{\text{vehicle}} (N, v) + 2 \text{ dB}$



- *ASEP Measurements* (Blue)
- *ASEP Measurements* (Red)

- Description of F/D proposal and J Proposal
- **Limit line(s) instead of Limit Points –
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Some important elements for each proposal

Japan Proposal :

- Lpmax vs. rpm axis,
- Using simple line as limit
- Reducing time to do ASEP Test

F/D Proposal :

- Take into account the gap between vehicle noise gear i and vehicle noise gear i-1 (or gear i-2) due to tyre noise contribution
- Using continuous measuring device, V max and N max at Lpmax to be more precise and to take into account of downshift,

Limit line(s) basis idea

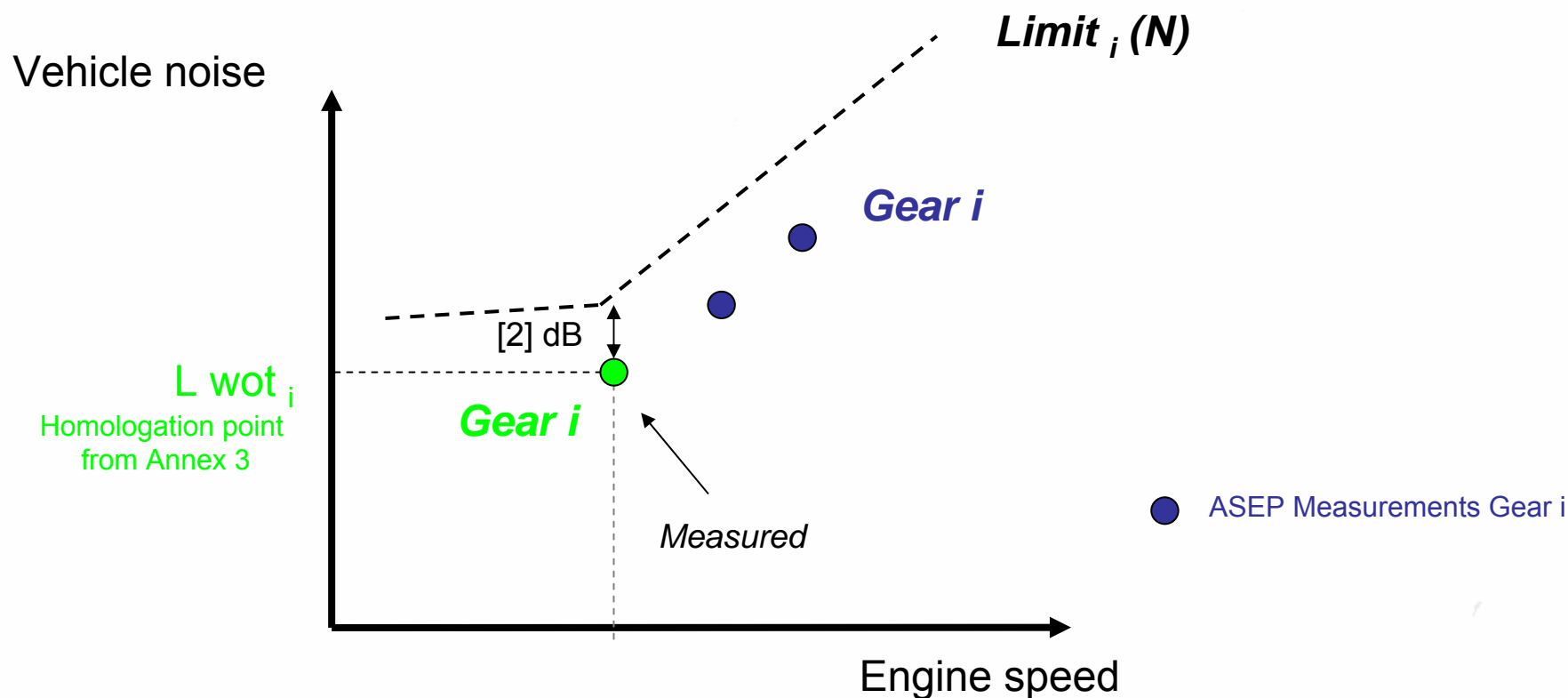
- L_{pmax} vs. rpm axis,
- Using simple line(s) as limit instead of points
- Take into account the gap between vehicle noise gear i and vehicle noise gear $i-1$ (or gear $i-2$)
- Reduce tyre noise measurements by measuring only L tyre 50 kph
- Using continuous measuring device, V_{max} and N_{max} at L_{pmax} to be more precise and to take into account of downshift,

Limit line(s) concept

ASEP measurements only on Gear i :

- For manual and automatic transmission with constant gear ratios tested only on Gear i for ASEP
- For CVT

→ **Line limit concept for Gear i : $Limit_i(N)$**

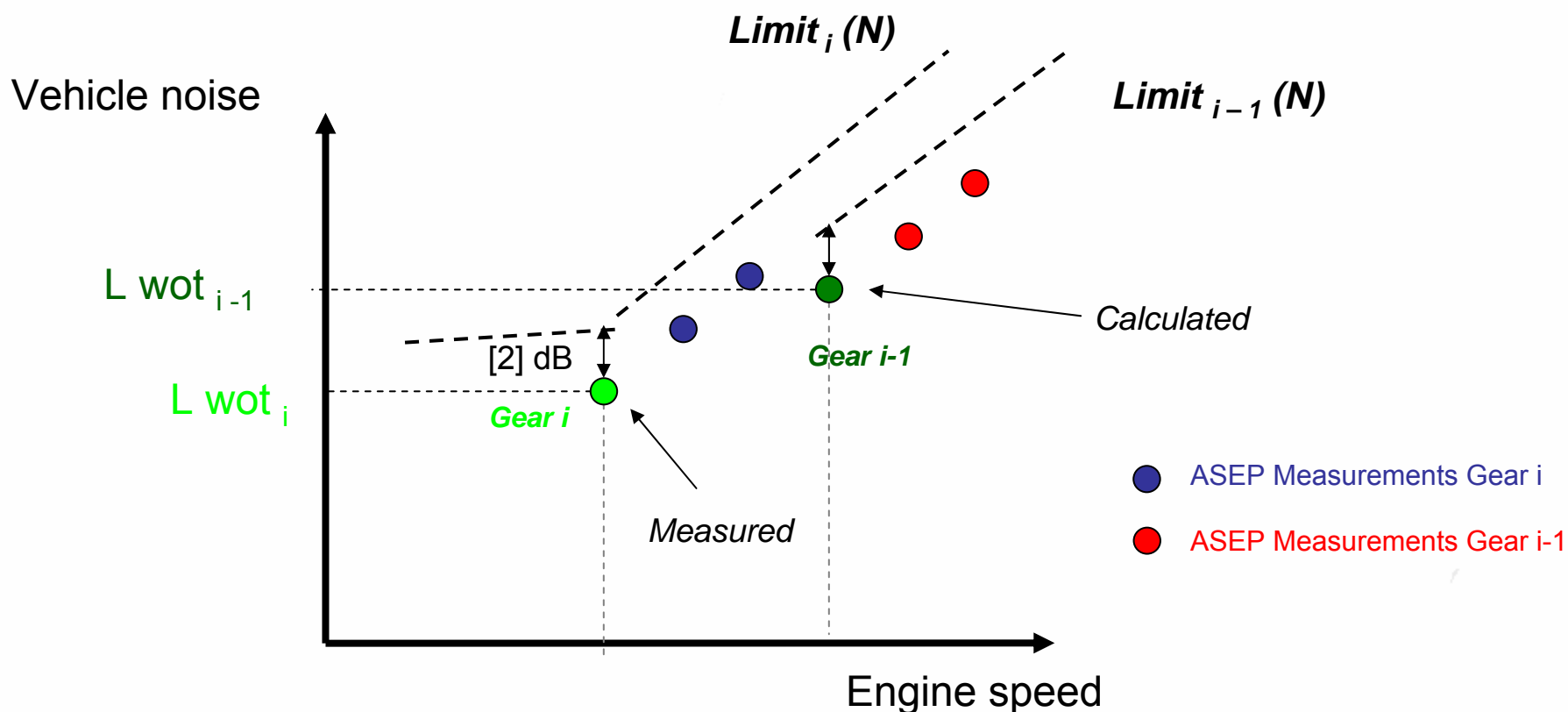


Limit line(s) concept

ASEP measurements only on Gear i and Gear i-1 :

- For manual and automatic transmission with constant gear ratios tested on Gear i, gear i-1 (and gear i-2 if necessary) for ASEP

→ Line limit concept for Gear i : $Limit_i(N)$



Line limit concept for Gear i : $\text{Limit}_i(N) = L \text{ wot}_i + b (N - N_i) + 2 \text{ dB}$

Line limit concept for Gear i-1 : $\text{Limit}_{i-1}(N) = L \text{ wot}_{i-1} + b (N - N_{i-1}) + [x]\text{dB}$

Line limit concept for Gear i-2 : $\text{Limit}_{i-2}(N) = \dots$

with $b = [6] \text{ dB} / 1000 \text{ rpm}$ for $N > N_i$ and $b = [3] \text{ dB} / 1000 \text{ rpm}$ for $N < N_i$

→ $L \text{ wot}_{i-1}$ is **calculated** by $L \text{ wot}_i$ and $L \text{ tyre } 50 \text{ kph}^*$

Determination of $L \text{ wot}_{i-1}$:

Basis datas : $L \text{ wot}_i$ from Annex 3 and additional measurements $L \text{ tyre } 50 \text{ kph}^*$

$$L \text{ wot}_{i-1} = [L \text{ engine } (N_i) + b (N_{i-1} - N_i)] \ll + \gg [L \text{ tyre } 50 \text{ kph}]$$

with $L \text{ engine } (N_i) = L \text{ wot}_i \ll - \gg L \text{ tyre } 50 \text{ kph}$

N_i is engine speed at 50 kph* on gear i

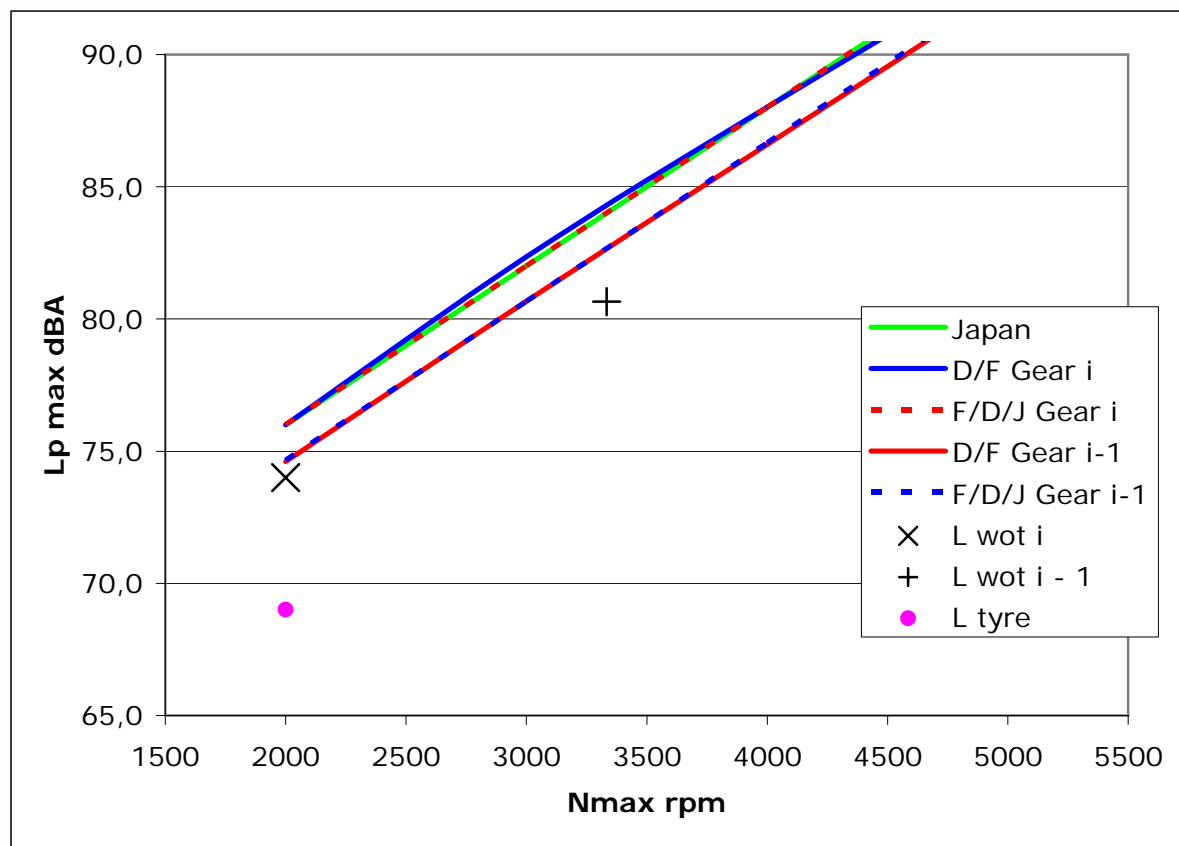
N_{i-1} is engine speed at 50 kph* on gear i - 1

* Nota : 50 kph can be in fact the real speed value $V_{L_{max}}$ at L_{max} ($L \text{ wot } i$)

Difference between F/D proposal and this limit line(s) concept

Comparison of D/F limit concept and this limit line(s) concept :

L wot i	74
N i	2000
L tyre 50	69
Tyre slope	40
ci	25
cj	15
Nj	3333
L engine i	72,3
L engine i-1	80,3
L wot i-1	80,7
slope vehicle	6

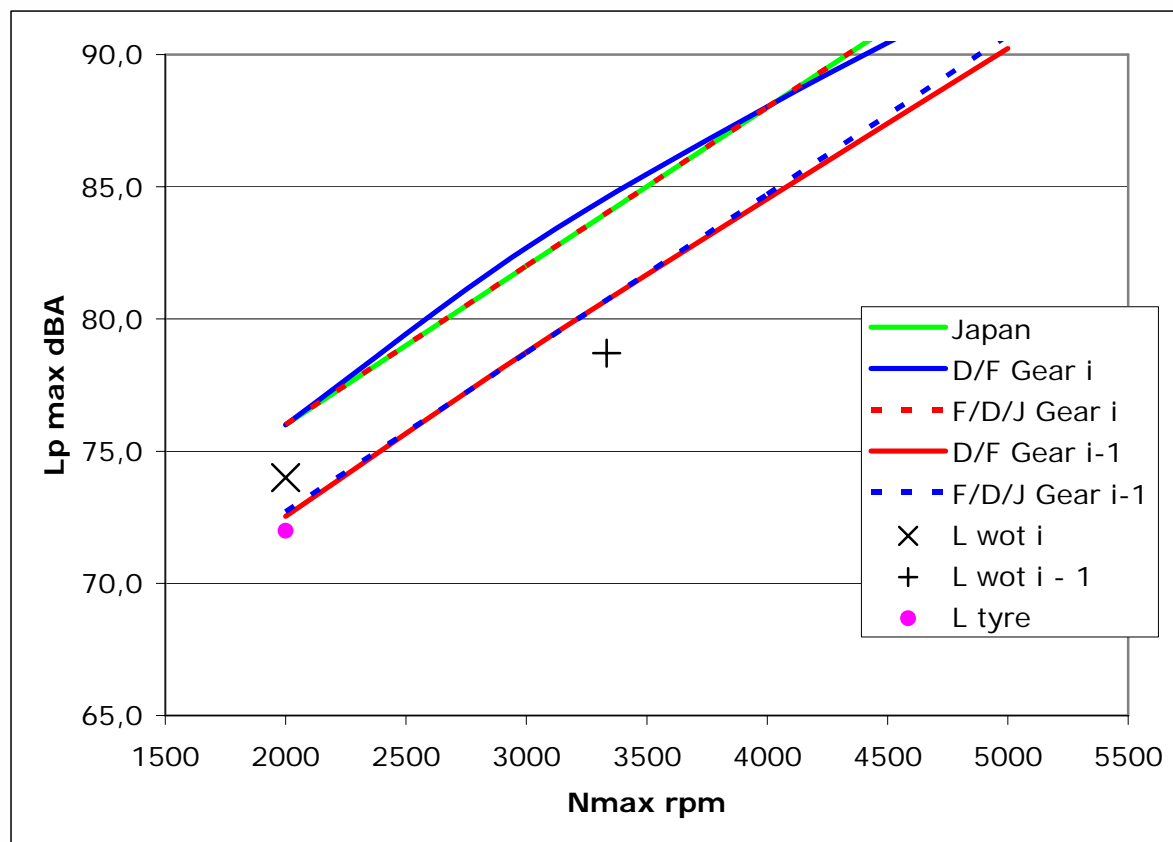


	Gear i		Gear i-1		Japan
	F/D/J	F/D	F/D/J	F/D	
2000	76,0	76,0	74,7	74,6	76,0
3000	82,0	82,4	80,7	80,7	82,0
4000	88,0	88,0	86,7	86,6	88,0
5000	94,0	93,4	92,7	92,5	94,0

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L wot i	74
N i	2000
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L engine i	69,7
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slope vehicle	6

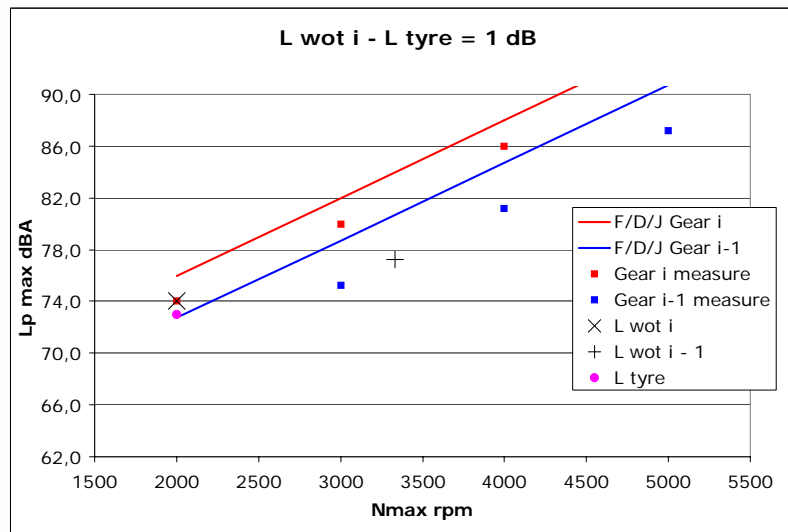
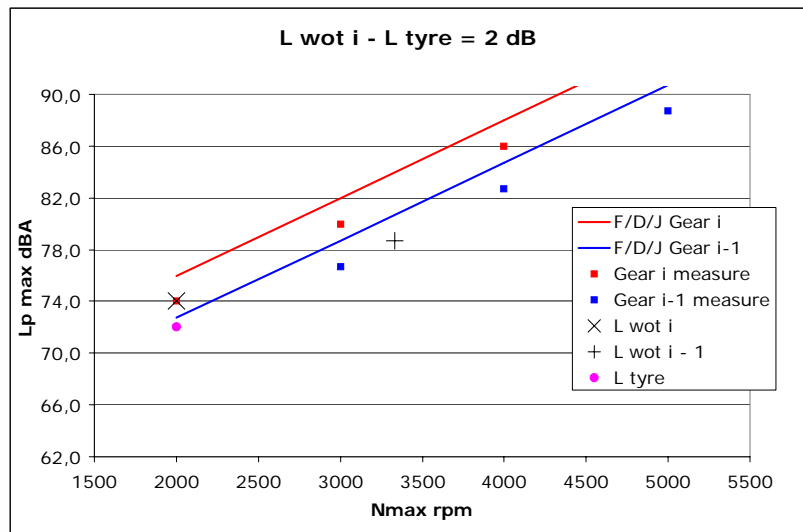
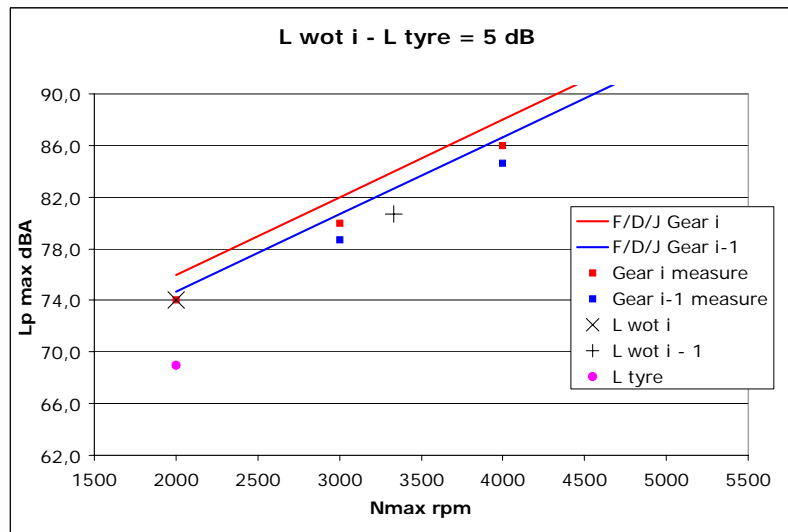
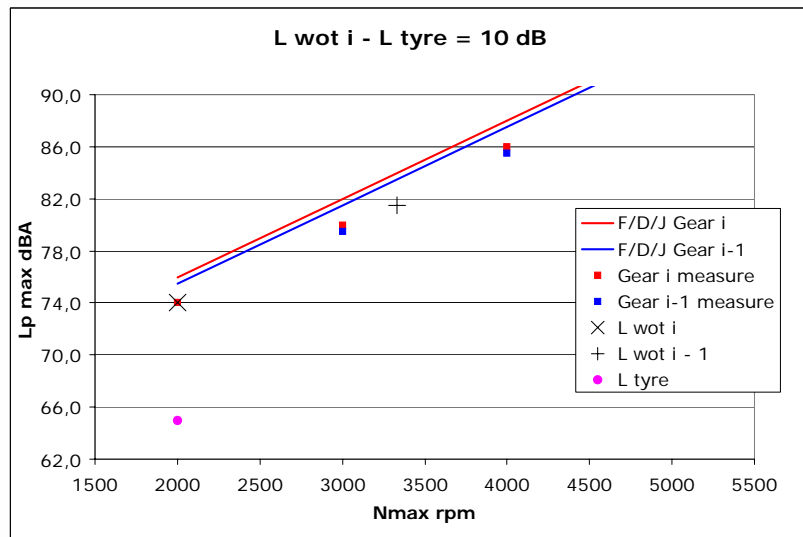


	Gear i		Gear i-1		Japan
	F/D/J	F/D	F/D/J	F/D	
2000	76,0	76,0	72,7	72,5	76,0
3000	82,0	82,7	78,7	78,7	82,0
4000	88,0	88,0	84,7	84,5	88,0
5000	94,0	92,8	90,7	90,2	94,0

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FOR VEHICLE NOISE CLOSE TO TYRE NOISE

For $L_{wot\ i} - L_{tyre50} < 2\text{ dB}$ \rightarrow L_{tyre50} is fixed to $L_{wot\ i} - 2\text{ dB}$



- It seems to be possible to simply F/D proposal to converge to Japan proposal on a simple model which take account of tyre noise with a quite good precision.
- It seems to be possible to take into account of tyre noise close to vehicle noise in the F/D proposal.
- More studying must be done to validate these approaches.
- One question to choose method :
Is « non linearity » level be in relation to audible trouble ?